

A Theoretical Analysis of Groundwater Flow in Small Drainage Basins¹

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Abstract. Theoretically, three types of flow systems may occur in a small basin: local, intermediate, and regional. The local systems are separated by subvertical boundaries, and the systems of different order are separated by subhorizontal boundaries. The higher the topographic relief, the greater is the importance of the local systems. The flow lines of large unconfined flow systems do not cross major topographic features. Stagnant bodies of groundwater occur at points where flow systems meet or branch. Recharge and discharge areas alternate; thus only part of the basin will contribute to the baseflow of its main stream. Motion of groundwater is sluggish or nil under extended flat areas, with little chance of the water being freshened. Water level fluctuations decrease with depth, and only a small percentage of the total volume of the groundwater in the basin participates in the hydrologic cycle.

Introduction. Whereas it is important to have a *general understanding* of the motion of groundwater in dealing with groundwater problems, the careless and frequent use of the expression may subvert its basic meaning. Until certain characteristics of the flow systems involved are well defined, groundwater motion in a given area cannot be conceived to be generally known. Among the numerous features, a knowledge of which is indispensable to the understanding of groundwater motion in an area, the following are thought to be the most important: the locations and extent of recharge and discharge areas, the direction and velocity of flow at any given point in the region, and the depths of penetration of the flow systems. It is easy to appreciate the value of this information if one considers only the difficulties which may arise in connection with problems such as outlining areas of potentially equal yield, tracing contaminants, estimating baseflow of rivers, and establishing groundwater budgets.

The purpose of this paper is to present a theory by means of which groundwater flow in small drainage basins can be analyzed. Some of the properties of flow derived from this analysis are obvious and may be observed in the field,

but others are hidden and may not be revealed even by expensive test programs. The neglect of these latter properties could lead to entirely wrong conclusions regarding groundwater flow in small basins either in general or in any particular case. Even if the theory is not used to obtain quantitative results, the qualitative application may still contribute to the general understanding of groundwater flow in small basins.

Before starting with the development of the theory a brief account will be given of the reasons why a theoretical analysis is believed to be best suited for an initial general study of groundwater flow in a given area.

General. The methods of studying groundwater motion can be either practical or theoretical. The group of practical methods includes field investigations based on the principles of geology, geophysics, geochemistry, and hydrology, and it is thus based on observations of phenomena controlling or related to the flow of groundwater in nature. The theoretical methods, on the other hand, make use of electrical analogs, scale models, and mathematical models to investigate phenomena resulting from idealized situations. In the final analysis the conclusions drawn from the data of both groups should be considered, and they must be in agreement. Nevertheless, the writer believes the results obtained by the application of the theoretical methods to be the more useful in the initial

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stages of an investigation. This view is based on the presumption that an observed phenomenon is usually related to only one feature of a given flow system, whereas it might be brought about by different causes in different situations; it may be the identical particular solution of several problems.

A few examples may prove helpful in clarifying this statement. For instance, a decrease in hydraulic head with depth, commonly observed in water wells, may be produced either by head losses due to the vertical downward-component of the water motion or by the water being perched in the permeable layers of a geological formation consisting of a series of more and less pervious beds [Meinzer, 1923, p. 41]. Another good example is a perennial body of impounded surface water. It may owe its existence either to poor underground drainage due to geologic conditions or to continuous groundwater discharge caused by the general pattern of the flow systems. The cause of a relatively low baseflow yield for a river may be even more uncertain because it could be explained by a basin-wide low permeability, by good surface drainage, or by the stream not being the only place of groundwater discharge in the basin. It is realized, of course, that the larger the variety of independent investigations, the more precisely the characteristics of the flow can be outlined. There

still may remain the uncertainty, however, of whether some of the decisive features have been overlooked and whether there may be some characteristics that cannot be measured at all. Whereas it is practically impossible to observe separately all phenomena connected with a regime of groundwater flow, a correct theory discloses every feature and draws attention to the most important properties of the flow.

It is believed that small drainage basins are the most important units in the groundwater regime. A good understanding of groundwater movement in adjacent small basins makes possible an accurate representation of the motion of groundwater within the large basin that they form. In working from larger basins to smaller basins the weight of the uncertainties increases, and a vague and possibly unreliable analysis is obtained. Apart from this, a small basin is commonly much less complicated than a large basin with respect to geology and topography; therefore, it lends itself much better to both practical and theoretical studies.

The definition of a small drainage basin as it will be understood throughout this paper is: *an area bounded by topographic highs, its lowest parts being occupied by an impounded body of surface water or by the outlet of a relatively low order stream and having similar physiographic conditions over the whole of its surface.*

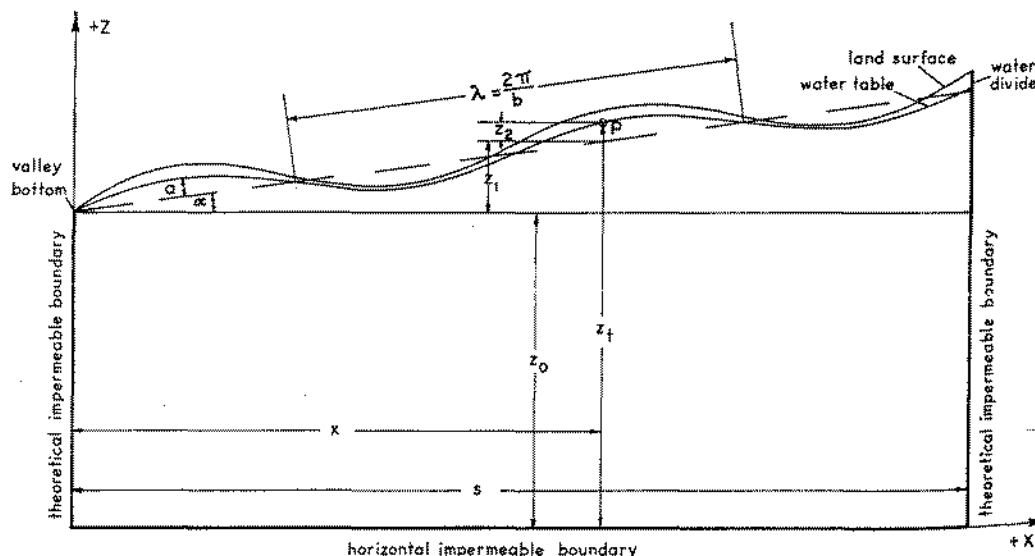


Fig. 1. Idealized cross section of a valley flank in a small drainage basin.

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The upper limit of area for such basins is usually several hundred square miles.

Mathematical development. In the mathematical analysis the region of groundwater flow at one side of the valley is represented by a rectangular area (Figure 1). This area is limited by a horizontal impermeable boundary at its base, by two vertical impermeable boundaries extending downward from the stream and the water divide, and by a horizontal line at the elevation of the stream along which line the fluid-potential distribution is supposed to be the same as that for the real water table. The assumption of a horizontal impermeable boundary as the lower limit of the basin is justified because, in the interval above this in which no such boundary is known, all groundwater belongs to the flow region of the basin. If, however, a relatively impermeable boundary is present underlying the whole basin, the water systems under it will not significantly interfere with the systems within the basin. The assumption of the two vertical boundaries is, strictly speaking, correct only if the surface drainage pattern is symmetrical—that is, if the basin is bounded by two parallel and equally removed surface-water divides of equal topographic elevation. In this case the potential distribution at both sides of the stream is symmetrical and the impermeable boundaries may be drawn vertically at the stream and at the divides. It will be shown later that a small amount of asymmetry in the topography does not cause a significant deviation from the vertical of these boundaries.

The potential distribution along the theoretical surface, although identical with that of the water table, is along a horizontal surface, and this restricts the validity of the numerical results to small slopes of about 3° or less. For the topography within the basin, a sinusoidal shape has been chosen, the highs and lows of which are thought to be representative of the hills and depressions of the natural land surface.

The analysis is also based on the assumption that the geologic conditions in the basin are isotropic and homogeneous. Whether or not this assumption is justified depends on the extent to which a real case deviates from the ideal conditions.

The assumption that the problem can be treated as a two-dimensional one is supported by the recognition that in most small basins the

slopes of the valley flanks greatly exceed the longitudinal slopes of the valley floors. This difference in slope causes the longitudinal component of the flow to become negligible compared with the lateral component.

The distribution of the fluid potential in a basin with boundaries as outlined above is derived from the general expression for the fluid potential [Hubbert, 1940, p. 802]:

$$\phi = gz + \int_{p_0}^p \frac{dp}{\rho} \quad (1)$$

where ϕ = fluid potential, g = acceleration due to the earth's gravity field, z = elevation above the horizontal impermeable boundary as standard datum, p_0 = pressure of the atmosphere, p = pressure in the flow region at any point, ρ = density of water.

If the water table is defined as a specific piezometric surface in the groundwater region at which the gravity potential is a maximum and the pressure potential equals that of the atmosphere, (1) reduces to

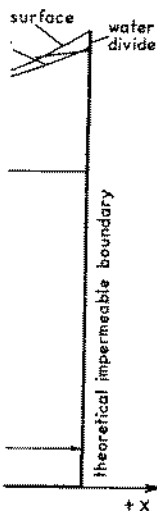
$$\phi_1 = gz_1 \quad (2)$$

for the water table, where z_1 = the topographic elevation of the water table at any point in the basin. It has been observed in Alberta [Meneley, 1963, pp. 4-12] as well as elsewhere [King, 1892, pp. 15-18; Meinzer, 1923, p. 34; Wisler and Brater, 1959, Figure 85; Wieckowska, 1960, p. 64] that the water table is generally similar in form to the land surface. Thus z_1 is found to consist of three components: z_0 , z_1 , and z_2 (Figure 1). z_0 is a constant, denoting the depth to the horizontal impermeable boundary from the stream bottom. $z_1 = x \tan \alpha$, where x is the horizontal distance of any point in the flow region from the valley bottom and α is the average slope of the valley flank. As long as α is small, z_2 may be approximated by

$$z_2 = a \frac{\sin (bx/\cos \alpha)}{\cos \alpha}$$

where a is the amplitude of the sine curve, $b = 2\pi/\lambda$ is the frequency, and λ is the period of the sine wave. With the three components known, the equation of the water table is obtained:

$$z_1 = z_0 + x \tan \alpha + a \frac{\sin (bx/\cos \alpha)}{\cos \alpha}$$



Upon introducing the abbreviations $\tan \alpha = c'$, $a/\cos \alpha = a'$, and $b/\cos \alpha = b'$, the final form of z_i is written as

$$z_i = z_0 + c'x + a' \sin b'x \quad (3)$$

From (2) and (3) the potential at the water table is found:

$$\phi_i = g(z_0 + c'x + a' \sin b'x) \quad (4)$$

Owing to the natural equilibrium of the ground-water budget in a basin, the average level of the water table is assumed to be constant. The problem is thus a steady-state potential problem which may be solved by applying the Laplace equation:

$$\partial^2 \phi / \partial x^2 + \partial^2 \phi / \partial z^2 = 0$$

The four boundary conditions will be as follows:

$$\partial \phi / \partial x = 0 \quad \text{at } x = 0 \text{ and } s$$

$$\text{for } 0 \leq z \leq z_0 \quad (5a, 5b)$$

$$\partial \phi / \partial z = 0 \quad \text{at } z = 0 \text{ for } 0 \leq x \leq s \quad (5c)$$

$$\phi_i = g(z_0 + c'x + a' \sin b'x) \quad \text{at } z = z_0$$

$$\text{for } 0 \leq x \leq s \quad (5d)$$

where s is the horizontal distance between the valley bottom and the water divide.

The general solution of the Laplace equation can be written in the following form:

$$\phi = e^{-kz}(A \cos kx + B \sin kx) + e^{kz}(M \cos kx + N \sin kx)$$

The arbitrary constants A , B , M , and N can be found from the boundary conditions.

Upon performing the derivation we get the following final equation for the fluid potential:

$$\begin{aligned} \phi = & g \left\{ z_0 + \frac{c's}{2} + \frac{a'}{sb'} (1 - \cos b's) \right. \\ & + 2 \sum_{m=1}^{\infty} \left[\frac{a'b'(1 - \cos b's \cos m\pi)}{b'^2 - m^2 \pi^2 / s^2} \right. \\ & \left. + \frac{c's^2}{m^2 \pi^2} (\cos m\pi - 1) \right] \\ & \left. - \frac{\cos(m\pi x/s) \cosh(m\pi z/s)}{s \cdot \cosh(m\pi z_0/s)} \right\} \quad (6) \end{aligned}$$

Equation 6 satisfies both the boundary conditions and the Laplace equation. By means of

Darcy's law, (6) can be used to obtain the specific mass discharge in the direction of r [Hubbert, 1940, p. 842].

$$j_r = -\rho \sigma \partial \phi / \partial r \quad (7a)$$

or the total flow vector:

$$\mathbf{j} = -\rho \sigma \text{grad } \phi \quad (7b)$$

where $\sigma = k\rho/\eta$ (k = coefficient of permeability, η = viscosity of fluid).

Numerical computations. To analyze the effect of the geometry of the basin on the ground-water flow, (6) has been solved for various parameters. To facilitate visualization of the flow, the numerical values of the potential are expressed in 'head of water above standard datum.' The potential distributions and flow patterns for the various cases are shown in Figures 2a to 2i.

The horizontal distance between the water divide and the valley bottom is 20,000 feet in all computed cases. This distance seems to be fairly representative for the half-width of a small basin.

Three values have been assumed for the depth to the impermeable boundary at the valley bottom: 1000, 5000, and 10,000 feet. The 1000-foot case is likely to be encountered in nature, whereas a relatively homogeneous body of sediment 10,000 feet thick is a rather hypothetical case. Flow patterns have, however, been evaluated for this situation, for several reasons: first, it represents an extreme case, and therefore the general validity of the conclusions arrived at by employing (6) can be checked; second, the general features of the flow patterns are more conspicuous in the deeper boundaries than in the shallow ones; and third, the measure that is the most characteristic in determining the potential distribution is the ratio $n = (z_0/s)$ of the depth of the impermeable boundary to the horizontal distance between divide and stream. By employing the three values of z_0 , a wide variety of potential distributions for values of n up to 0.5 can be inferred at least qualitatively.

Flow systems in small basins based on interpretation of the mathematical results. Upon inspection of Figures 2a to 2i we recognize a certain grouping of the flow lines. (In the figures the solid lines are called lines of force. Under isotropic conditions the lines of force coin-



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$$\partial r \quad (7a)$$

$$\phi \quad (7b)$$

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Results based on interval results. Upon 20 ft we recognize a line. (In the figures of force. Un- lines of force coin-

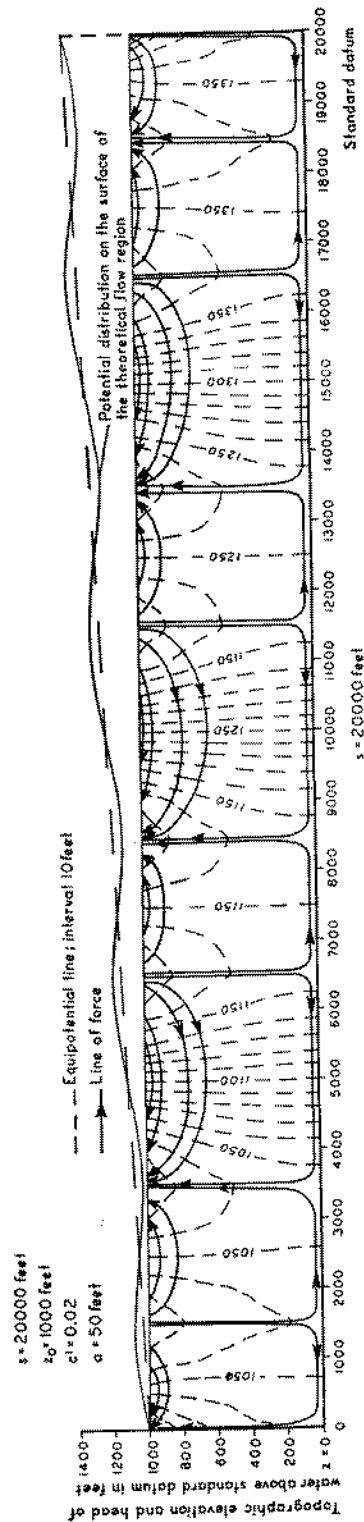


Fig. 2a. Potential distribution and flow pattern as obtained by equation 6.

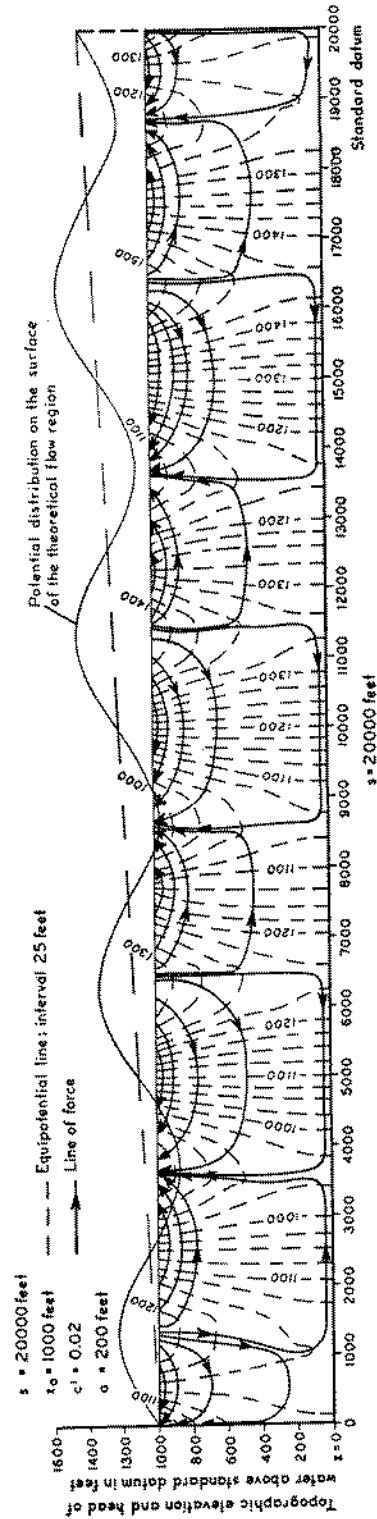


Fig. 2b. Potential distribution and flow pattern as obtained by equation 6.

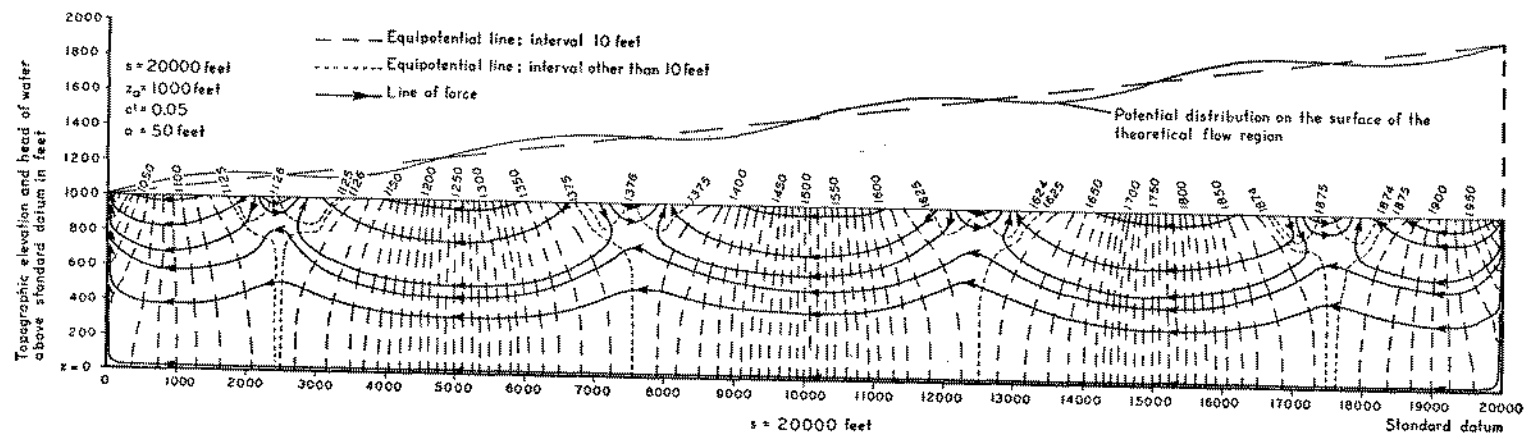


Fig. 2c. Potential distribution and flow pattern as obtained by equation 6.

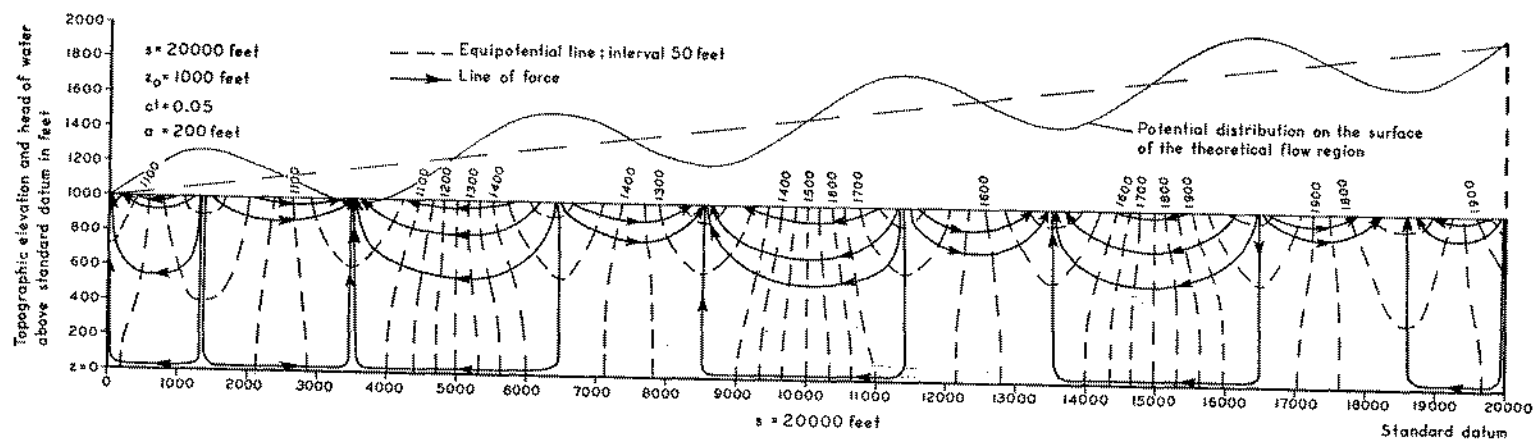
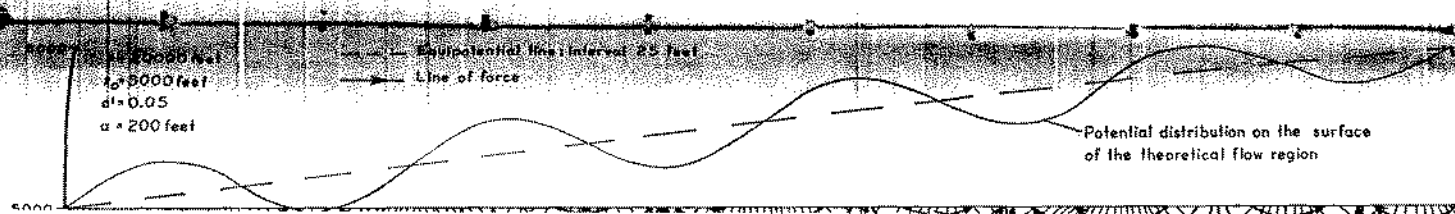


Fig. 2d. Potential distribution and flow pattern as obtained by equation 6.



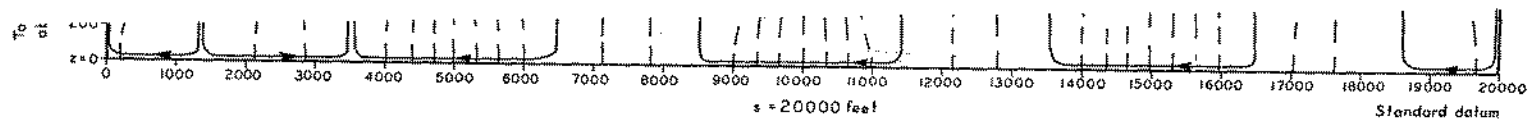


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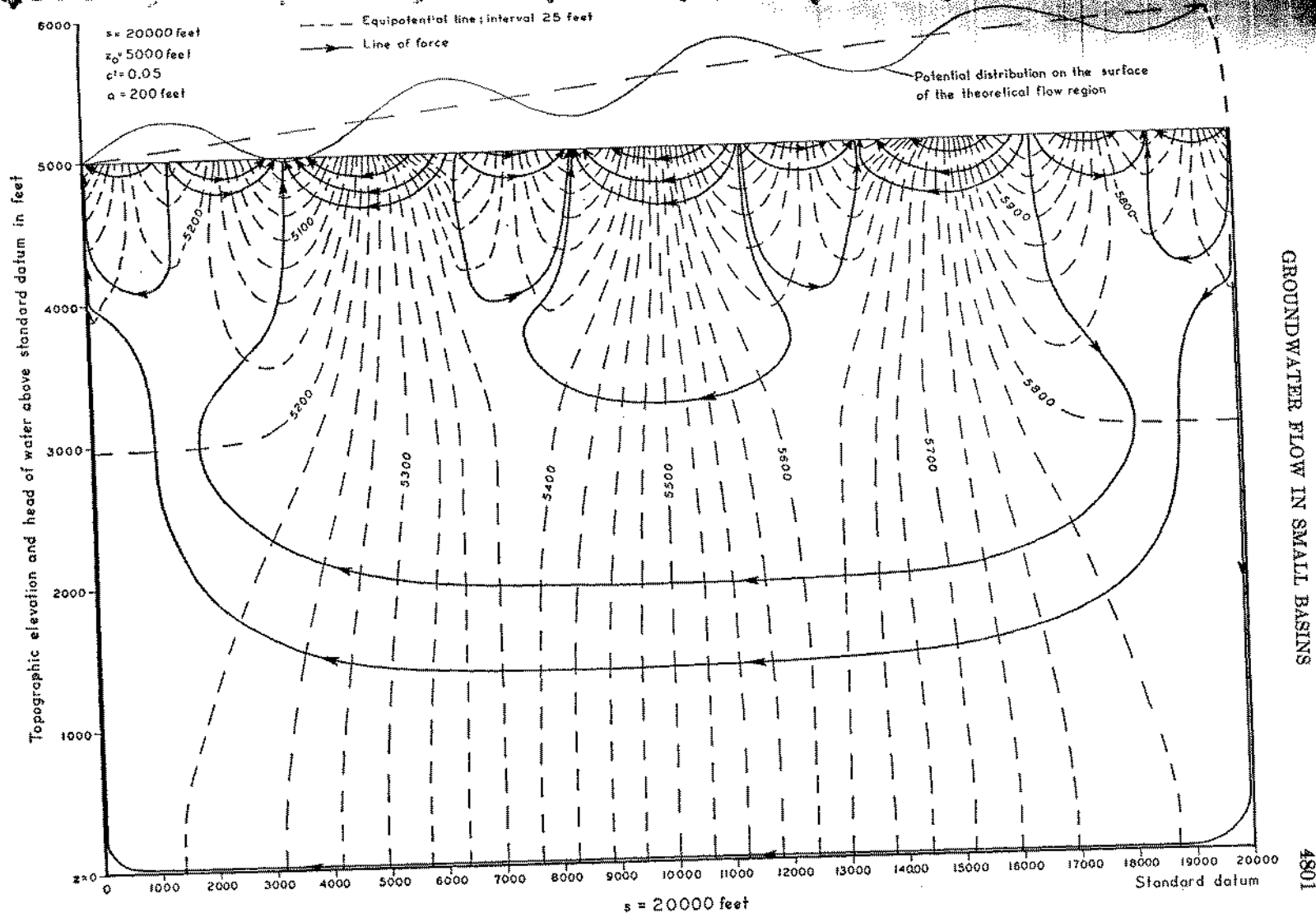


Fig. 2e. Potential distribution and flow pattern as obtained by equation 6.

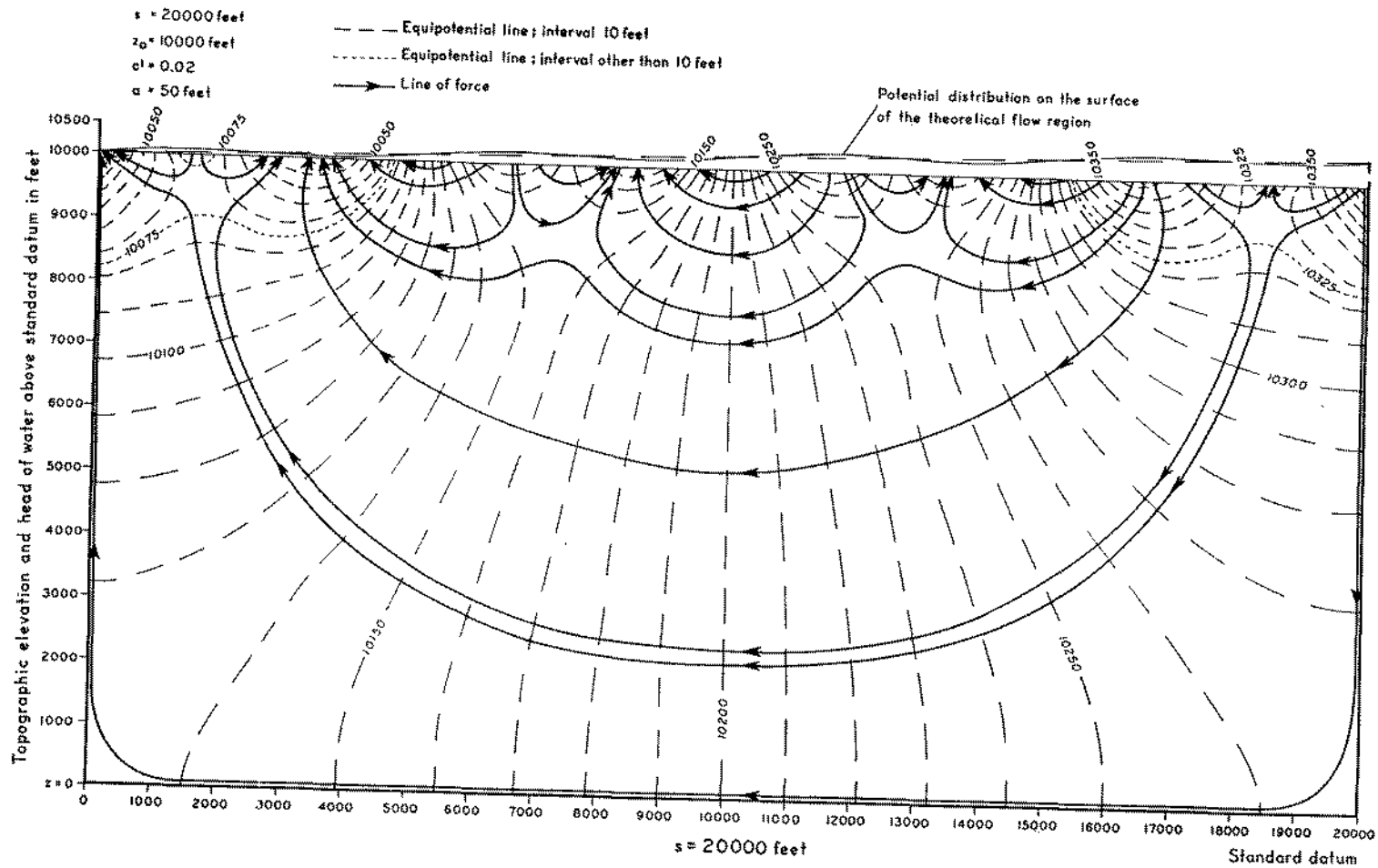


Fig. 2f. Potential distribution and flow pattern as obtained by equation 6.

$s = 20000$ feet
 $z_0 = 10000$ feet
 $c^1 = 0.02$
 $a = 200$ feet

--- Equipotential line; interval 25 feet
 → Line of force

Potential distribution on the surface of the theoretical flow region

0 1000 2000 3000 4000 5000 6000 7000 8000 9000 10000 11000 12000 13000 14000 15000 16000 17000 18000 19000 20000
 $s = 20000$ feet
 Standard datum

Fig. 2f. Potential distribution and flow pattern as obtained by equation 6.

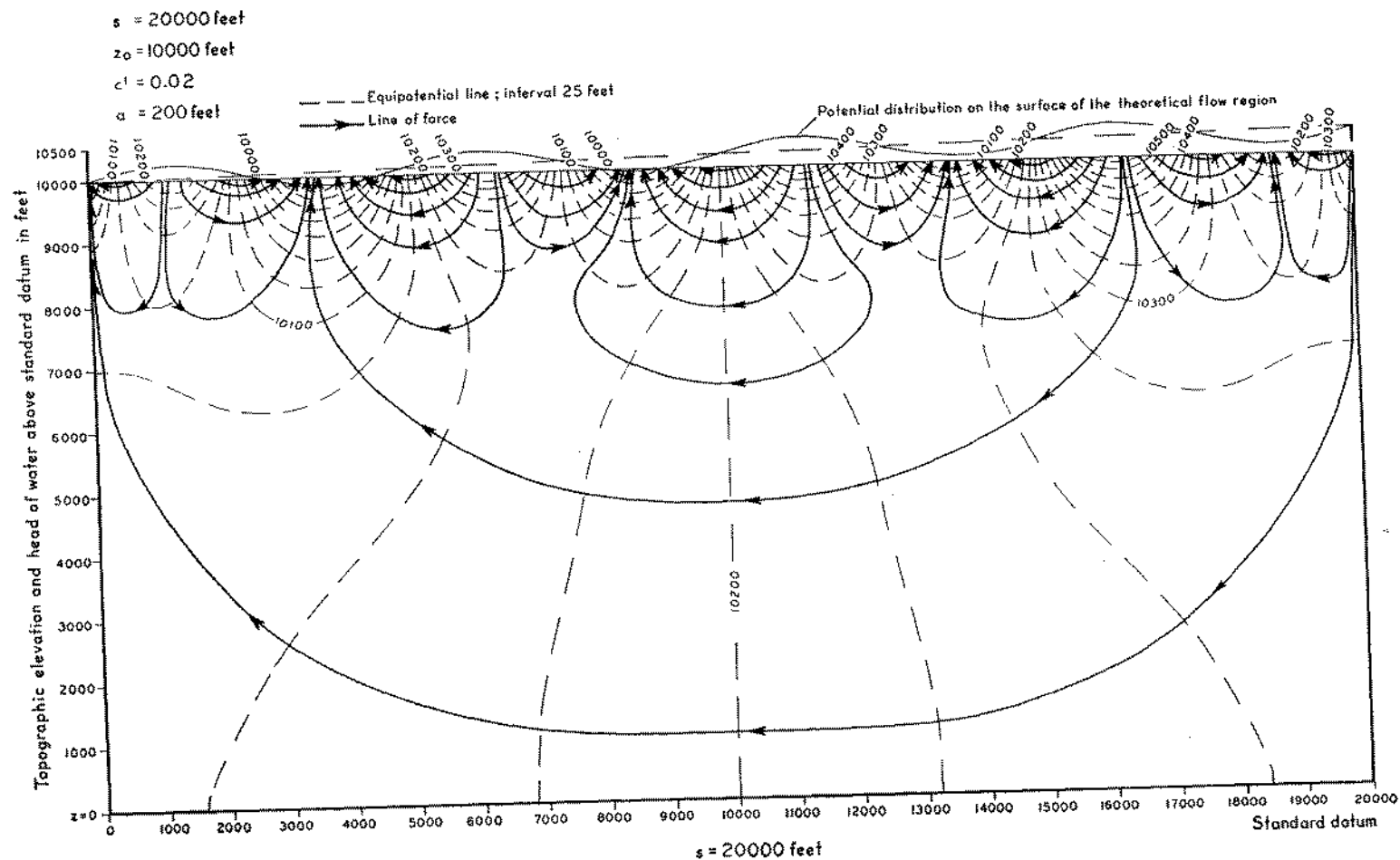


Fig. 2g. Potential distribution and flow pattern as obtained by equation 6.

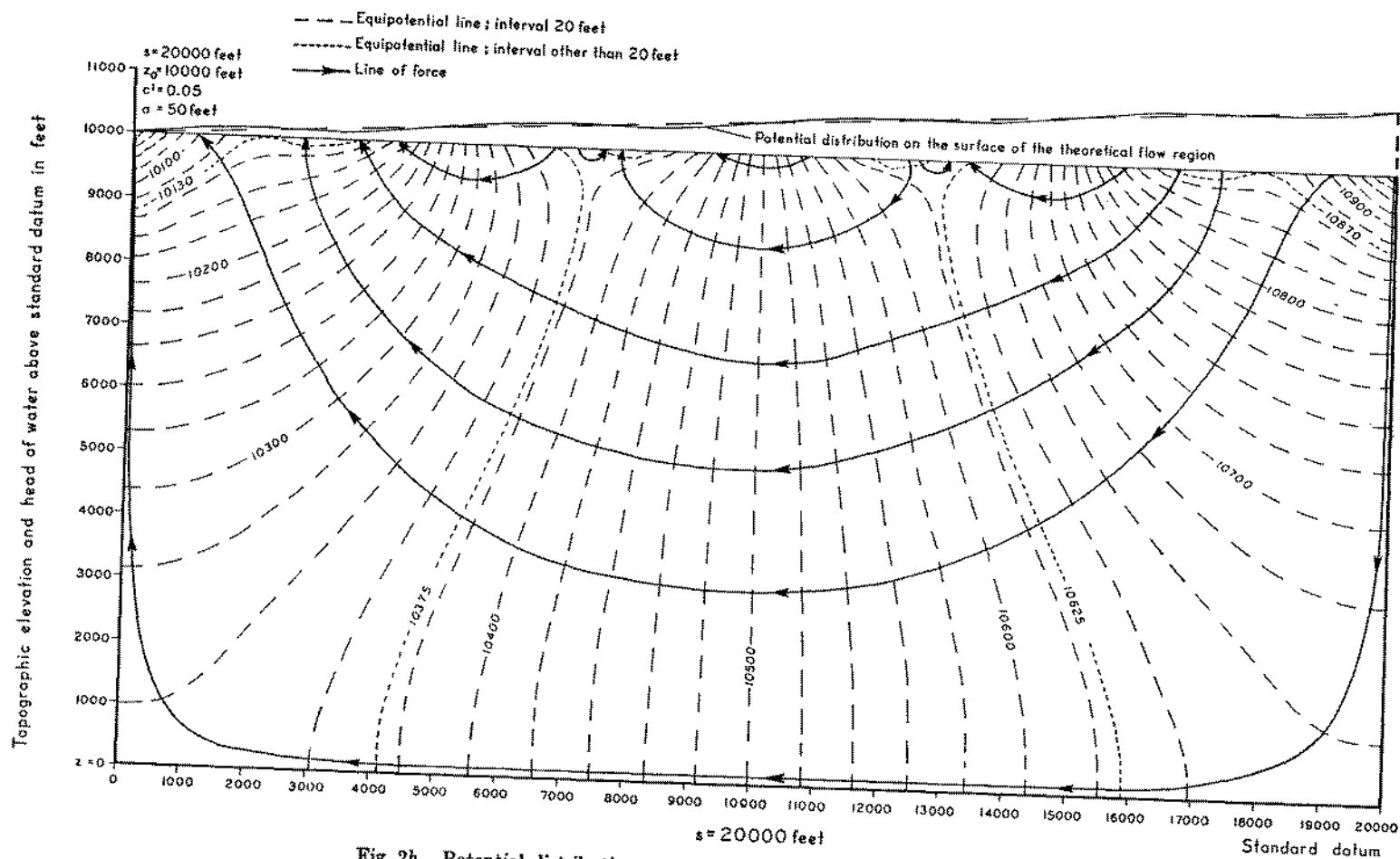
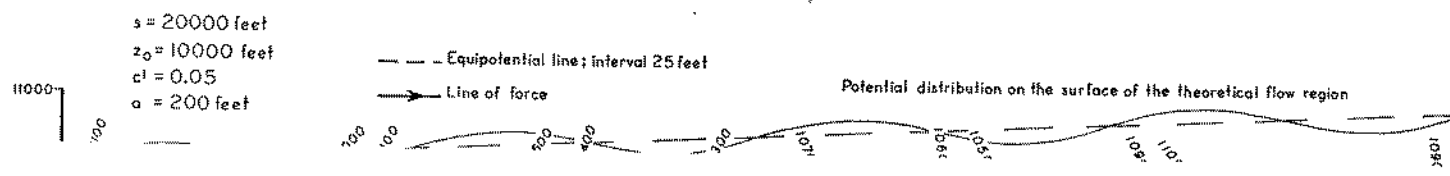


Fig. 2h. Potential distribution and flow pattern as obtained by equation 6.



cide with the flow lines.) Such a group of flow lines is said to form a flow system if it satisfies the following definition: *a flow system is a set of flow lines in which any two flow lines adjacent at one point of the flow region remain adjacent through the whole region; they can be intersected anywhere by an uninterrupted surface across which flow takes place in one direction only.*

Further investigation of the figures shows that three distinctly different types of flow systems can occupy a basin, namely, local, intermediate, and regional systems (Figure 3). A *local system* of groundwater flow has its recharge area at a topographic high and its discharge area at a topographic low that are located adjacent to each other. Local systems can be readily observed on each diagram of Figure 2. The major characteristic of an *intermediate system* of groundwater flow is that, although its recharge and discharge areas do not occupy the highest and lowest elevated places, respectively, in the basin, one or more topographic highs and lows may be located between them. Very well-defined intermediate systems can be seen in Figures 2e, f, g, h, and i. The apparent lack of intermediate systems in those cases for which z_0 is 1000 feet does not mean that no such systems may exist in basins of relatively shallow depth. As soon as the real land surface departs from the regularity of the sine curve, the symmetrical flow pattern of Figure 2c, for instance, will be somewhat modified, and flow will occur between intermediate highs and lows also. A system of groundwater flow is considered to be *regional* if its recharge area occupies the water divide and its discharge area lies at the bottom of the basin. Regional systems can be observed in all the deep cases and in Figure 2c, where z_0 is 1000 feet.

Whereas theoretically the boundaries between different flow systems are very well defined, they do not signify an abrupt change of any of the physical properties of the flow. Relatively rapid changes of the chemical composition of the water across the boundaries, however, could be expected because of the different locations of the recharge and the different lengths of the flow paths of the different systems. In a small basin of moderate relief the amount of recharge water is directly proportional to the area of recharge. With this in mind it is obvious from

Figure 2 that the greatest flow-line densities are found at shallow depths of the local systems. Except at places where local stagnant bodies of water occur, the density of the flow lines decreases rapidly with depth and with the transition from the local to the intermediate region and reaches its minimum in the regional system, provided the latter exists.

This interpretation of the theoretical results is very much in agreement with views expressed by *Norvatov and Popov* [1961, p. 21]. They recognize 'three well pronounced vertical zones of groundwater flow':

1. 'upper zone of active flow, whose geographical zonality coincides with climatic belts. The lower boundary of this zone coincides with the local base levels of rivers;
2. 'medium zone of delayed flow, subject to lesser climatic effect but also geographically zonal. The lower boundary of this zone is the base level of large rivers;
3. 'lower zone (of relatively stagnant water), geographically azonal and lying below the base level of large stream systems.'

Taking into account the extent of the recharge areas of the regional systems (which are small relative to those of the local systems), we see that flow in the regional system is influenced by climatic effects to a much lesser degree than flow in the upper zone. Climatic or geographical zonality is, therefore, a straightforward consequence of the present theory.

In the next few paragraphs an analysis will be given of the effects of geomorphological factors on the flow of groundwater. These factors, or parameters in (6), are (a) the ratio n of the depth z_0 to the impermeable boundary to the half-width s of the basin (for convenience, in discussing the effect of n , only the depth to the impermeable boundary will be referred to, s being the same in all cases); (b) the average slope of the valley flanks; and (c) the local relief.

In analyzing the effect of z_0 on the flow of groundwater, a comparison of the diagrams of Figure 2 is helpful. Let those diagrams be considered for which all parameters but z_0 are equal, for instance, Figures 2d, e, and i. It appears that the spacing of the equipotential lines is *closer* in the shallow case than in the deeper ones. The flow lines are more arcuate as depth

Boundary between flow systems of different order
Boundary between flow systems of similar order
Line of force

$s = 20000$ feet
 $z_0 = 10000$ feet
 $c^1 = 0.02$
 $a = 50$ feet

Potential distribution on the surface of the theoretical flow region

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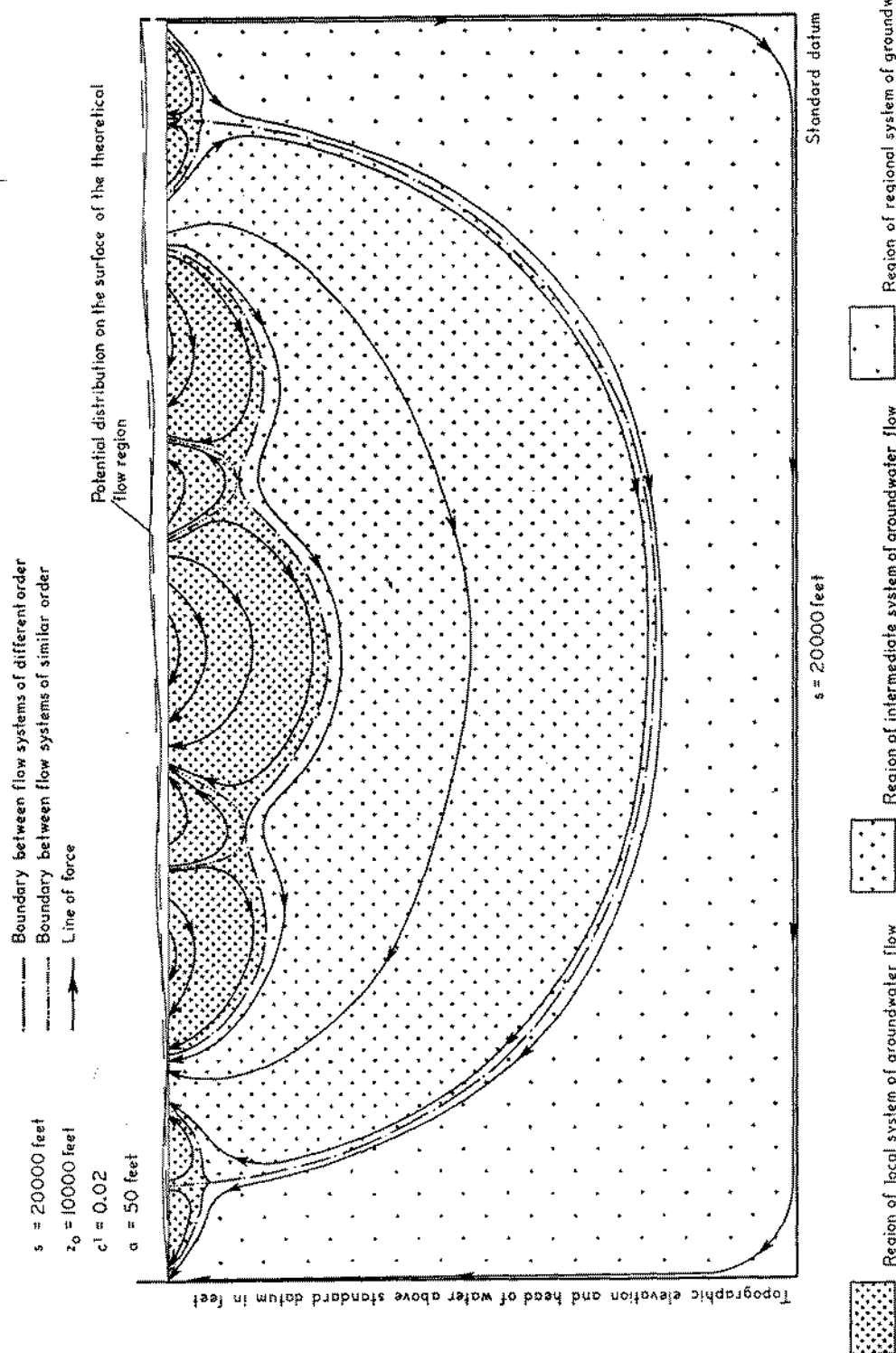


Fig. 3. Theoretical flow pattern and boundaries between different flow systems.

increases and there is room for intermediate and regional systems to form in those cases for which z_0 is 5000 or 10,000 feet. These features indicate a more evenly distributed flow, therefore a less intense motion if z_0 increases. A comparison of Figures 2c and 2h shows that a regional system is also possible in a relatively shallow case but that, with other parameters remaining the same, a much larger amount of water is transmitted through the regional system if z_0 is large. To summarize the effect of z_0 on the flow system it can be stated that, as the depth of the flow region increases, the water movement will slow down. A slow motion will probably result in higher mineralization of the groundwater.

A general increase in the slope of the valley flank will result in an increased lateral flow toward the bottom of the valley. The surficial areas of those systems whose flow lines are directed toward the center of the basin extend, and those of the other systems decrease. Local flow systems may degenerate to stagnant areas and may even vanish, thus allowing intermediate or regional systems to form. Figures 2a, 2c, 2f, and 2h illustrate this change well. Owing to the generally increased velocity of motion, a larger range of fluctuation of the piezometric surface is to be expected for the steeper slope of the valley flank.

Increasing topographic relief will tend to increase the depths and the intensities of the local flow systems. Whereas in Figure 2c a well-developed regional flow system is observed, in Figure 2d the entire basin is occupied by local systems. The depth ranges of the local system in Figure 2f are approximately 1000 feet shallower than those in Figure 2g. In the extreme case where the relief is negligible no local systems will form. However, since well-defined local flow systems are found even with the relatively low relief of approximately 100 feet per 2500 feet (a gradient of 0.04), neglecting their existence in theoretical or practical problems can hardly be justified.

Consequences of the theory. The major features of groundwater flow and flow systems derived from the theory presented here will be discussed in the following paragraphs.

1. Recalling the effects of the general slope and local relief on the flow, we see that under extended flat areas groundwater movement is

retarded; neither regional nor local systems can develop. Groundwater may be discharged only by evapotranspiration; discharge of this type will possibly result in water-logged areas. If a relation between mineralization of the water and velocity of flow can be assumed, water in those areas will have high concentrations of soluble salts.

2. If the local relief is negligible and if there is a general slope only, a regional system will develop. Theoretically, if the line located on the surface midway between and parallel to the valley bottom and the water divide is called the 'midline,' the recharge and discharge areas of this regional system are located between the midline and divide, and between the midline and valley bottom, respectively [Tóth, 1962]. Because of the decreasing velocities, a gradual increase of dissolved mineral constituents with depth is to be expected. A good example of potential distribution and flow pattern in this situation has been produced by measurements in Long Island, New York, in connection with attempts to solve contamination problems. Figure 4 shows the results of the measurements [Geraghty, 1960, p. 38].

3. If the topography has a well-defined relief, local flow systems originate. The higher the relief, the deeper are the local systems. At the boundary between two adjacent systems the flow is subvertical and downward or upward in direction. Such a boundary is located under the highest and lowest elevated parts of local hills and depressions, respectively. Thus, whereas in the basin the underground drainage is not strictly symmetrical, imaginary impermeable boundaries may be thought to be located at local lows and highs, at least to the depths of the local systems. Figure 5 is a good example of an inferred local system [Back, 1960, p. 94].

4. The very pronounced effect of the relief on the formation of local systems suggests that no extended, unconfined regional systems of flow can extend across valleys of large rivers or highly elevated watersheds.

5. As a result of the local systems, alternating recharge and discharge areas are found across a valley. This means that the origins of waters obtained from closely located places may not even be related. Rapid change in chemical quality may thus be expected.

6. At points where three flow systems meet

local systems can be discharged only in the large of this type of the logged areas. If a portion of the water is assumed, water in the intrusions of solu-

gible and if there is a regional system will be located on the divide parallel to the divide is called the recharge areas of the divide between the divide and the midline and [Toth, 1962]. Because of a gradual constituents with a good example of pattern in this situation measurements in connection with the problems. Figure 4 shows measurements

of a well-defined aquifer. The higher local systems. At present systems the divide or upward in the divide located under the divide parts of local divide. Thus, where the divide drainage is not very impermeable so be located at the divide depths of the divide good example of [Toth, 1960, p. 94]. The effect of the relief divide suggests that the divide systems of flow divide large rivers or

systems, alternative areas are found at the divide origins of the divide places may change in chemical

flow systems meet

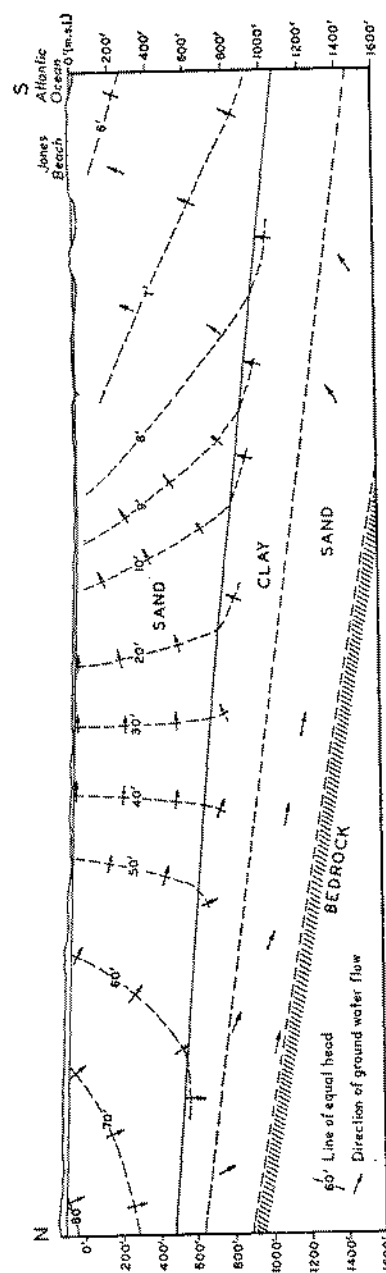


Fig. 4. North-south pattern of groundwater flow in southeastern Nassau County, Long Island, New York [after Geraghty, 1960].

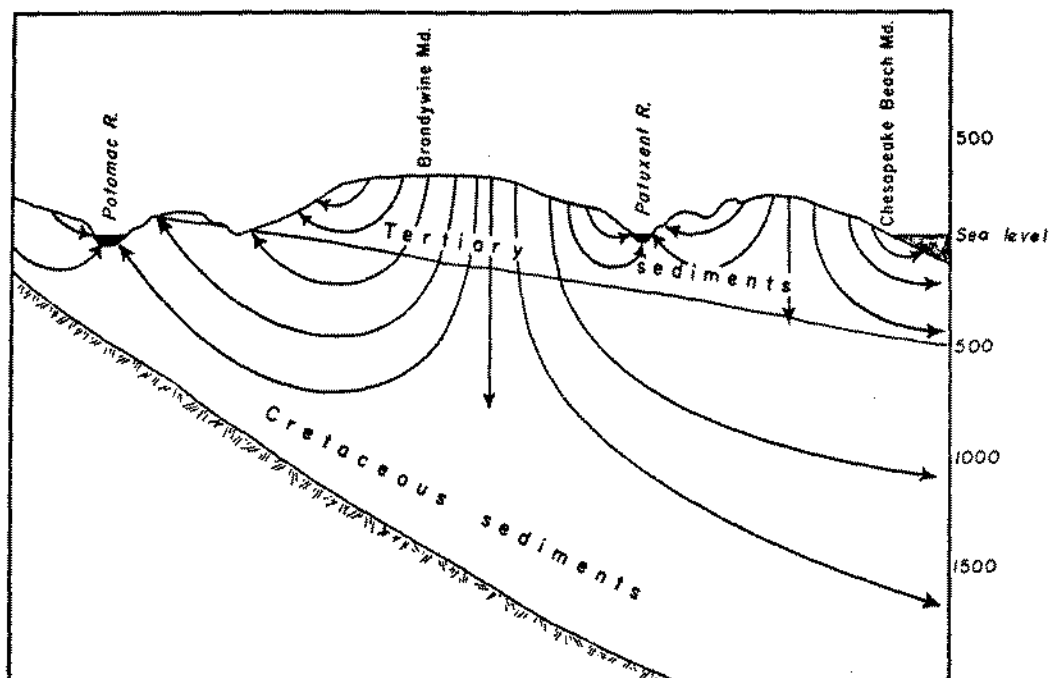


Fig. 5. Diagrammatic cross section through southern Maryland showing the lines of groundwater flow [after Back, 1960].

(Figure 2c), an area of stagnant water is formed. A high accumulation of mineral constituents is probable at these places. Below such a stagnant body of groundwater, flow occurs again and may result in a better quality of water than that from shallower depths.

7. Decreasing potential with depth in recharge areas and increasing potential in discharge areas are direct consequences of the theory and can be observed in all diagrams of Figure 2. It should be noted, however, that such a configuration of the equipotential lines is pronounced only in the immediate vicinities of the highs and lows. The midlines and their vicinities are locations of relatively straight, vertical equipotential lines.

8. From Figure 2 it can safely be stated that the major stream of the basin receives groundwater contributions only from the adjacent topographic highs and from possible regional flow. The latter is probably unimportant in most cases because of the low rate of flow. It is conceivable, then, that the methods in which baseflow data are used for computation of basin-wide characteristics (average recharge, permeability, etc.) are misleading or erroneous. Even

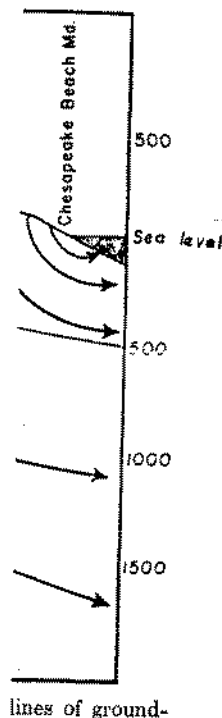
if the two flanks of a basin are of low relief, so that there are no local systems, the bulk of the basin discharge will take place between the midline and the valley bottom and only a small portion will appear as baseflow.

9. A further consequence of the theory is that the water levels at shallow depths are the most affected by seasonal recharge and discharge. The small intake and outlet areas of the intermediate and regional zones prevent the water levels from fluctuating widely. Plotnikov and Bogomolov [1958, p. 90] make a distinction between two zones on the basis of fluctuation of the water levels. They call the first 'zone of oscillations of underground water levels.' According to them the volume of water that occupies the zone of oscillation undergoes seasonal variations. This volume would control groundwater discharge and therefore they call it 'control reserves of underground waters.' Their second zone includes all the water that is below the zone of oscillation, both that in the deeper, still homogeneous parts of the basin and that in artesian aquifers; these are the 'secular resources.' It seems that the 'zone of oscillation' and the portion of the 'secular resources' that

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is above the first impermeable boundary coincide very well with the 'local systems' and with the 'intermediate and regional systems' of the present paper.

10. Another result of the analysis is that only a small portion of the total amount of water occupying the basin participates in the hydrologic cycle. The deeper the basin, the smaller is this portion. This is easily conceived when one considers that the greatest part of the surface of the basin is occupied by the recharge and discharge areas of local systems which are usually shallow. But even when the local systems reach the horizontal impermeable boundary (Figures 2a, b, d), approximately 90 per cent of the total recharge water never penetrates deeper than 250 to 300 feet. A similar view is expressed by Ubell [1962, p. 96] who believes that about 80 to 90 per cent of the 'static supply does not participate in the natural hydrological cycle.' His experiments, on the basis of which this conclusion was drawn, indicated that 'below a certain depth in loose sedimentary rocks . . . water does not move in the voids until their state of stress is disturbed by boring.'

Summary. It is the writer's belief that in drainage basins, down to depths at which basin-wide extended layers of contrasting low permeability are found, groundwater motion may be treated as an unconfined flow through a homogeneous medium. On the basis of this principle a mathematical model of a small drainage basin (as defined in the paper) has been constructed. Potential distributions have been computed for basins of different geometrical parameters. These computations have led to a number of conclusions regarding features of the groundwater flow.

In the most general case, groundwater flow in a basin can be thought to be apportioned among three types of flow systems, the regional, intermediate, and local systems. The three systems, being the results of combinations of three particular solutions of the Laplace equation, can be superimposed on one another. If the local variations in topography are negligible the flow consists of the combination of only two particular solutions, and no local systems occur. This case has been found in nature by Geraghty [1960] and has been theoretically treated in detail elsewhere [Tóth, 1962].

The emphasis in the present paper has been

on the general situation for which local topography plays a part in controlling groundwater motion. The distribution of the flow systems will, in turn, have its effect on the chemical quality of local occurrences of groundwater. The areally unrelated origin of local systems, associated with local topographic highs and lows, may result in abrupt changes in the chemical composition of relatively shallow groundwater. Vertical changes in quality may be the result of local stagnant bodies and of the vertical arrangement of different flow systems.

It is thought that (6) may be used for obtaining quantitative information about groundwater flow in an area, the surface of which can be approximated by a harmonic function. It is hoped also that the results of the above analysis will be useful in test programs planning well fields, solving pollution and tracer problems, making baseflow studies, and setting up water budgets.

Acknowledgments. I am greatly indebted to Messrs. R. Newton and P. Redberger, of the Petroleum Division, Research Council of Alberta, who adapted the flow equation described in the paper for solution by digital computer. Only the availability of the computer solutions made possible the derivation of the many flow diagrams.

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Abstract
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Discussion of a Paper by J. Tóth, 'A Theory of Groundwater Motion in Small Drainage Basins in Central Alberta, Canada'

STANLEY N. DAVIS

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Stanford, California

Tóth [1962] has developed a system of groundwater circulation (Figure 1) which is used to explain anomalous water levels observed in continental sediments of Alberta. Two of the important features of this system are a wide discharge face downslope from the 'mid-line' and a 'hinge point' of zero water-level fluctuation which is located at the 'mid-line.'

The development of flow systems can be of great assistance in our understanding of many of the complex problems of hydrogeology. It can also be very misleading unless care is used in relating theoretical results to field conditions. Unfortunately, Tóth has not taken into account some of the essential features of a real system of groundwater circulation. At least five major difficulties are apparent:

1. A separation of the recharge area from the discharge area at the mid-line is not possible if groundwater recharge takes place downslope from the line. This is self-evident because groundwater on the discharge side is flowing counter to the direction of potential recharge. Uniform recharge over the entire area would shift the line separating the recharge zone from the discharge zone into the bottom of the valley. The actual width of the discharge face would vary with the distribution and quantity of recharge but would never extend upslope as far as the middle of the flow field unless recharge mysteriously stopped downslope from the mid-line.

2. No mechanism exists for removing the water from the downslope side of the mid-line. According to three of Tóth's diagrams, the water table is about at the same depth over most of the basin; consequently, evapotranspiration loss from the groundwater should be more or less uniformly distributed and cannot be considered as a mechanism for localized discharge.

3. Tóth's flow pattern is possible only if unnatural distributions of either permeability or

recharge are assumed. Inasmuch as the medium is isotropic and homogeneous by definition, only the peculiar recharge variation will be inspected. Tóth's Figure 3a is redrawn in Figure 1. Only one-third of the original equipotential lines are shown, but the configuration is identical to the original. The discharge, Q , in each flow channel is approximated by

$$Q = Kw \Delta m (\Delta h / \Delta s)$$

where K is the hydraulic conductivity, Δs is the length of the flow path within the segment of the flow net, Δh is the head drop between equipotential surfaces, Δm is the width of the segment of the flow net, and w is the thickness of the flow system perpendicular to the plane of the diagram. If the effective porosity, as well as w , K , and Δh , is constant, the groundwater recharge per unit area must be directly proportional to Q/x which in turn is proportional to $\Delta m/x\Delta s$, where x is the horizontal outcrop width of each flow channel. The relative recharge and discharge calculated in arbitrary units from Tóth's Figure 3a are shown in Figure 1. Although not calculated, the recharge pattern necessary to produce the flow system in Tóth's Figure 3b would indicate a much greater concentration of flow at the vertical boundaries of the system.

4. The 'hinge point' is impossible with the postulated fluctuations, namely, that the crest area is subject to large water-level fluctuations while 'two relatively stable points are at the valley bottom and at the mid-line' (p. 4383). This is the same as saying that the potential can be changed in one part of the flow field without changing the configuration of the equipotential surfaces throughout the field. This is possible only with nonsteady-state flow, which is not considered in Tóth's analysis.

5. Depth to water and total depth of wells

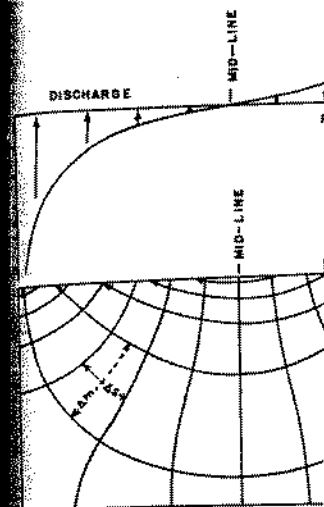


Fig. 1. Tóth's flow pattern with the required discharge and recharge.

are not related directly to the zone of saturation. Confusion is evident in Tóth's discussion and in the statements '... 2

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ied. Inasmuch as the medium is heterogeneous by definition, only a single variation will be inspected. The figure is redrawn in Figure 1. Only the original equipotential lines are shown. The configuration is identical to the original, Q , in each flow channel.

$$Kw \Delta m (\Delta h / \Delta s)$$

hydraulic conductivity, Δs is the vertical path within the segment of the flow, Δm is the width of the flow net, and w is the thickness of the aquifer perpendicular to the plane of the flow, the effective porosity, as well as the constant, the groundwater area must be directly proportional to the discharge in turn is proportional to the discharge. The relative recharge is indicated in arbitrary units from 0 to 1.0 are shown in Figure 1. Allocated, the recharge pattern indicates the flow system in Tóth's Figure 5. It indicates a much greater concentration at the vertical boundaries of the flow.

point' is impossible with the conditions, namely, that the crest of the large water-level fluctuations are stable points are at the crest at the mid-line' (p. 4383). In saying that the potential can be a part of the flow field without the configuration of the equipotential lines in the field. This is possible in steady-state flow, which is not the case in Tóth's analysis. The water and total depth of wells

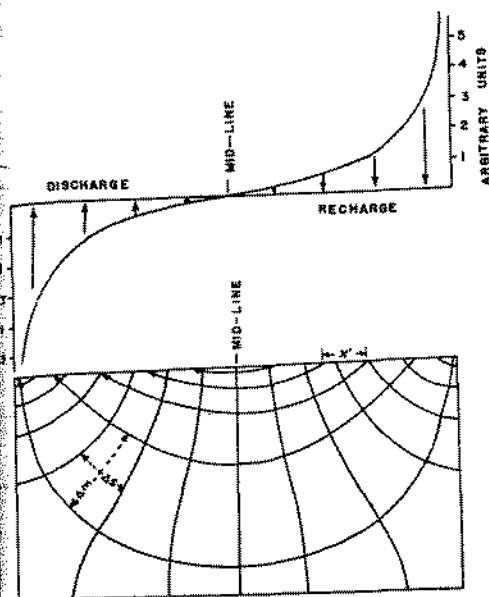


Fig. 1. Tóth's flow pattern for a valley side with the required discharge and recharge distribution.

are not related directly to the potential field in the zone of saturation. Confusion on this point is evident in Tóth's discussion of his Figure 5 and in the statements '... $\partial\phi/\partial x$ which is di-

rectly related to the slope of the topography ...' (pp. 4385-4386) and 'The piezometric surface observed in wells of approximately the same depth generally follows the topography because the flow is essentially unconfined.' (p. 4386), and 'Minor topographic irregularities may have their own associated flow systems ...' (p. 4386). The configuration of the water table, and hence of the potential field, is only affected by the topography where it influences the recharge or discharge of groundwater. Contrary to Tóth's inferences, the water table can commonly rise under small dry valleys which concentrate recharge from storm runoff. Tóth's Figure 5 only demonstrates that deeper water tables require deeper wells. A more refined interpretation must depend on further study of casing records, elevation of the water table in each of the areas, elevation of the water levels in the wells compared with the water table, further details of the local geology, and estimates of groundwater recharge.

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(Received November 13, 1962.)

Reply¹

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In his discussion Davis raises five points of criticism. I believe that his objections are brought about partly by a misunderstanding of some of the basic features of the theory and partly by possibly insufficient explanations given in the original paper. Whatever the cause may be, however, I hope that the following discussion will satisfactorily answer the points raised by Davis.

The first point of objection originates obviously from the regrettable lack of proper terminology regarding the processes involving recharge and discharge of groundwater. Without aiming at a complete classification of these processes a brief analysis of the terms *recharge* and *discharge* is given which should clarify the point raised by Davis. The terms are both generally used in two senses:

(a) The quantity of water that is added to or removed from the zone of saturation.

(b) The processes by which water is added to or removed from any part of the zone of saturation.

For the purposes of this discussion, it is necessary to consider (b) only. The processes of recharge and discharge may be subdivided into two main groups:

(1) Processes in which water is exchanged between the saturated zone and either the atmosphere or the zone of aeration.

(2) The process in which water is exchanged between different parts of the saturated zone. This process is termed herein 'the saturated flow of groundwater.'

Cross-sectional areas in which the saturated flow is inward with respect to the flow region, i.e. away from the water table, are generally

known as 'recharge areas,' and cross-sectional areas with saturated flow outward with respect to the flow region, i.e. toward the water table, are commonly designated 'discharge areas.' However, these same terms are used also to describe the direction of the water exchange between the zone of saturation and the atmosphere or the zone of aeration. Unfortunately, the dual meaning of these terms often leads to confusion. Such is apparent in Davis' first point. By recharge he appears to mean the process by which water obtained from precipitation is added to the zone of saturation, the long-term average of which is conceivably uniform over the entire area of a small basin. He argues then, that 'uniform recharge over the entire area would shift the line separating the recharge zone from the discharge zone into the bottom of the valley.' This argument implies that the entire area should be called a 'recharge area,' and that no line of separation can be present in case of uniform recharge. The separation between recharge and discharge areas is made in the original paper, however, on the basis of the direction of groundwater flow in a vertical plane. Thus, it is quite possible to have water derived from precipitation infiltrating through the zone of aeration toward the water table in areas where the direction of groundwater flow is upward, i.e. toward the water table, and in order for the midline to exist between an area of downward flow and an area of upward flow it is not necessary for recharge to be 'mysteriously stopped.'

Answers to the objections raised by Davis in his second, third, and fourth points have to be based on a very important condition, namely, that the theory gives the *long-term average* of the potential distribution. The theory does not yield quantitatively transient configurations of the flow pattern and of the water table. This basic property of the theory has been pointed out in the paper by my statement, for instance,

at 'the mean position of the water table, the average of that of many dry and many wet years will closely follow the topography' (p. 10). To find the general distribution of the potential, we disregard the initial potential, which the region is becoming saturated during the later transient periods of recharge during wet and dry seasons. Qualitative conclusions have been reached, regarding the nature of the flow of the water table. The method of arriving at these conclusions is elucidated in the figures and graphs in a more detailed manner in the original paper.

Davis' third point and the accompanying figures 1 and 2 are, in fact, quantitative. The first point was said on page 4382, near the bottom of the valley. . . . The flow distribution means that the water table is maximum at the divide. . . . owing to the assumed constant recharge of the water table, the theoretical amount of recharge water is the same at any other part of the basin. . . . The following mechanisms will cause the water table to increase if going from the valley toward the water divide. First, the evapotranspiration during dry years is less over the relatively deep water table in the valley than at the divide. . . . the divide means that more water is available from the unsaturated zone in the valley than in the divide. . . . region of saturated flow in the divide is toward flow than in areas close to the valley. Second, a relatively large amount of available precipitation can infiltrate in the divide than in the valley. . . . are far removed from the center of the valley than in the divide. . . . stream. This must be so because the divide is close to the stream. . . . the surface reaches the stream. . . . infiltrate. Owing to the longer travel time, however, during which the water travels from remote parts of the divide to the stream, the time enough for a large portion of the water to infiltrate. The increased infiltration in the divide relative to that at the valley is a mechanism is treated in detail in (1961, pp. 21 and 23). Support of these conclusions by thousands of experiments on the development of infiltration' he developed infiltration which he employs the concept of

¹ Contribution no. 201 from the Research Council of Alberta.

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recharge areas,' and cross-sectional flow outward with respect to the water table, i.e. toward the water table designated 'discharge areas.' How these terms are used also to describe the water exchange between the ground and the atmosphere or the ground surface. Unfortunately, the dual meanings often leads to confusion. Such as Davis' first point. By recharge he means the process by which water or precipitation is added to the zone of long-term average of which is the water table over the entire area of a basin. He argues then, that 'uniform recharge over the entire area would shift the line of discharge from the divide to the bottom of the valley.' This argument is based on the entire area should be recharged, and that no line of separation exists in case of uniform recharge between recharge and discharge areas. In the original paper, however, on the direction of groundwater flow in the valley. Thus, it is quite possible to have recharge from precipitation infiltrate into the zone of aeration toward the divide where the direction of flow is upward, i.e. toward the divide. In order for the midline to exist, there must be downward flow and an area of discharge is not necessary for recharge to be stopped.' objections raised by Davis in his third and fourth points have to be considered an important condition, namely, the long-term average of the distribution. The theory does not consider transient configurations of the water table. Thus the theory has been pointed out by my statement, for instance,

that 'the mean position of the water table, the average of that of many dry and wet seasons, will closely follow the topography' (p. 4380) or 'to find the general distribution of the fluid potential, we disregard the initial period during which the region is becoming saturated, as well as the later transient periods of recharge and discharge during wet and dry seasons' (p. 4381). Qualitative conclusions have been reached, however, regarding the nature of the fluctuations of the water table. The method of arriving at these conclusions is elucidated in the following paragraphs in a more detailed manner than in the original paper.

Davis' third point and the accompanying Figure 1 are, in fact, quantitative statements of what was said on page 4382, namely, 'Flow is most intense in the vicinity of the divide and at the bottom of the valley. . . . This type of flow distribution means that the decline of the water table is maximum at the water divide. Owing to the assumed constant average elevation of the water table, the theory calls for a larger amount of recharge water at the divides than at any other part of the basin. Each of the two following mechanisms will cause the recharge to increase if going from the valley bottom toward the water divide. First, the decreased rate of evapotranspiration during dry seasons owing to the relatively deep water table close to and at the divide means that more water can percolate from the unsaturated zone down to the region of saturated flow in the area of downward flow than in areas close to the bottom of the valley. Second, a relatively larger portion of the available precipitation can infiltrate in areas that are far removed from the central drainage channel of the valley than in areas adjacent to the stream. This must be so because from areas situated close to the stream the water running over the surface reaches the stream before it can infiltrate. Owing to the longer period of time, however, during which the water runs over the surface from remote parts of the basin, there is time enough for a large portion of the water to infiltrate. The increased infiltration at the water divide relative to that at the valley bottom and its mechanism is treated in detail by Befani [1961, pp. 21 and 23]. Supported by 'several thousand experiments on the determination of infiltration' he developed infiltration formulas in which he employs the concept of, for instance,

'the critical (maximum) capacity of the aeration zone near the ridge' (p. 23). In summary, it can be stated that whereas the distribution of recharge and discharge required by the theory [Tóth, 1962] and calculated by Davis may seem to be unconventional, it is probably not as unnatural as Davis conceives it in his third point.

Davis' second point has been answered partially by the foregoing discussion. The water table should be shown shallower in the vicinity of the creeks than at the highlands in all the diagrams. It is difficult, however, to show this properly on the scale used. The shallow water table results in a relatively high rate of evapotranspiration and in an increased amount of seepage. Also, the vicinity of the creek is the typical location of flowing wells and springs in Alberta. Numerous creeks are known with distances between their water divides not exceeding 6 miles and with valley bottoms over 1 mile in width. These bottoms are gently sloping and flat and have boggy, marshy surfaces during and even after the long, dry and hot summers that are common in the province. These phenomena are unmistakable indications of upwardly directed groundwater flow, and they provide an acceptable explanation of water removal from the downslope side of the midline.

The concept of the hinge point, refuted by Davis in his fourth point, is based on the theoretical consideration that the changes in the potential distribution on both sides of the midline are equal and of opposite direction during the winter, i.e. when recharge and discharge are limited owing to the frozen ground. Throughout this period the location of the hinge point must theoretically remain constant. During the other seasons, continuing upward flow and infiltration will counterbalance evapotranspiration and cause the water table to remain close to the surface in the lower parts of the basin, as is evidenced by the many marshy valley bottoms already mentioned. In the upper parts of the valley, on the other hand, the decline of the water table, caused partly by evapotranspiration but mainly by the downward component of the saturated flow, must be offset by infiltration within a few months in the spring in Alberta. Components of the phreatic fluctuation other than those due to the saturated flow will cause both vertical and horizontal shifting of the hinge point. However, the major consequence of a theoretical hinge point

is believed to be valid, namely that 'the phreatic belt must be wider at the upper half of the valley flank than between the midline and valley bottom' (p. 4383).

Davis' fifth criticism is directed against relations between the 'depth to water' or the 'total depth of wells' and the potential field. In Davis' opinion, attempts are made to establish these relations. Figure 5 is intended, however, to show the variation of the fluid potential with depth in the region of saturated flow. To this end the well depth has been used to determine the vertical position of the point in the flow region at which the potential is measured. This method of determining the vertical position appears to be justified because the well depth is usually representative of the depth of the zone from which the water is obtained. The fluid potential is expressed as the elevation of the nonpumping water level above a standard datum. Depths to nonpumping water levels are, therefore, indicative of the fluid potentials in the zones from which the water comes. Thus the increase in depth to the nonpumping water level as well depth increases, illustrated by the curve for re-

charge areas in Figure 5, shows that in areas of theoretical downward flow the measured potentials decrease with depth. Figure 5 and its discussion do not present conclusions regarding the relation between the elevation of the *water table* and the depth of the wells, but rather conclusions regarding the relation between the *fluid potential* and depth. This point apparently has been misunderstood by Davis, judging by his statement, 'Tóth's Figure 5 only demonstrates that deeper water tables require deeper wells.'

In conclusion it must be said that, whereas I disagree with the majority of the points raised by Davis, I am sincerely grateful for having been made aware of possible vagueness in my paper.

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It is generally accepted that sensations are retarded by a kin within the earth. The most fa the Fennoscandian uplift due nce of the Pleistocene ice shee ime t_r of the Fennoscandian up the deviation from isostasy din is value was about 5000 year here is the dependence of t_r on wavelength L . By a flow proces tell [1935, p. 36; see also Heis/ Meinesz, 1958, p. 369 and Jeffr is inversely proportional to L wavelength inequalities subside elusion, if accepted, will lead 1 Since the wavelength of the F lift is about 2000 km, the relax second harmonic in the gravity wavelength is about 20,000 kr the satellites, will be 500 years above relation between t_r and by O'Keefe [1959], this would ble sea transgressions up to 1 tury. Similar difficulties are papers. In his 1958 paper (p. 3 after a discussion similar to adopted a time constant of 10 and harmonic in the gravity 1 too short to be compatible wit al data. Munk and MacDona that the present ellipticity of sponds to an equilibrium bulg ago. This presupposes t_r to be is indicated by the $1/L$ relatic

In the present letter, we w tion to a flow process by which to the square of L . An excell this process is seen in Jeffrey just one page after that dealin process. In this process we m mediate layer in which viscous and the mathematical analys is similar to that of long wav trary to this, in the process di ginning of this letter, we need 1 mathematical analysis is simil face waves. Adopting the in process, however, we can over