

# march 6 lecture → examples

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- review steady-state condition for CSTR:

mass balance:

$$(\text{rate of mass accum}) = (\text{mass flux in}) - (\text{mass flux out}) \pm (\text{source/sink})$$

$$\frac{dC}{dt} \neq Q C_0 - Q C - k C A$$

sink, first order

@ S.S.  $\frac{dC}{dt} = 0$

$$0 = Q C_0 - Q C - k C A$$

$$0 = \frac{Q}{A} C_0 - \frac{Q}{A} C - k C$$

$$0 = \frac{C_0}{t_0} - \frac{C}{t_0} - k C$$

$$0 = \frac{C_0}{t_0} - C \frac{(1 + kt_0)}{t_0}$$

, note that  $\frac{A}{Q} = t_0 = \theta_H$   
is hydraulic residence time (pg 6-14)

$$\therefore C = \frac{C_0}{1 + kt_0}$$

• example, cascade of reactors (pg 6-26)

$\rho$ - denotes products

$C_{\rho i} = 30 \text{ g/m}^3$ , influent conc.

$r_p = -k C_p$ , first order decay

$$K = 0.2 \text{ d}^{-1}$$

$$Q = 5 \text{ m}^3/\text{s}$$

$$V_1 = 8.64 \times 10^5 \text{ m}^3$$

$$V_2 = 25.92 \times 10^5 \text{ m}^3$$

$$V_3 = 17.28 \times 10^5 \text{ m}^3$$

$$V_4 = 8.64 \times 10^5 \text{ m}^3$$

$$V_5 = 25.92 \times 10^5 \text{ m}^3$$

• solution

- Step 1 • assume system is at steady-state (i.e.  $dc/dt = 0$ )  
 • write mass balance equation for each reactor

$$\textcircled{1} \quad 0 = Q C_{\rho i} - Q C_{\rho 1} - k C_{\rho 1} V_1$$

$$\textcircled{2} \quad 0 = Q C_{\rho 1} - Q C_{\rho 2} - k C_{\rho 2} V_2$$

$$\textcircled{3} \quad 0 = Q C_{\rho 2} - Q C_{\rho 3} - k C_{\rho 3} V_3$$

$$\textcircled{4} \quad 0 = Q C_{\rho 3} - Q C_{\rho 4} - k C_{\rho 4} V_4$$

$$\textcircled{5} \quad 0 = Q C_{\rho 4} - Q C_{\rho 5} - k C_{\rho 5} V_5$$

Step 2 • rearrange equations

$$\text{from } \textcircled{1} \quad C_{\rho 1} = \frac{C_{\rho i}}{(1 + k \theta_{H_1})}$$

$$\text{from } \textcircled{2} \quad C_{\rho 2} = \frac{C_{\rho i}}{(1 + k \theta_{H_1})(1 + k \theta_{H_2})}$$

$$\text{from } \textcircled{3} \quad C_{\rho 3} = \frac{C_{\rho i}}{(1 + k \theta_{H_1})(1 + k \theta_{H_2})(1 + k \theta_{H_3})}$$

$$\text{from } \textcircled{4} \quad C_{\rho 4} = \frac{C_{\rho i}}{(1 + k \theta_{H_1})(1 + k \theta_{H_2})(1 + k \theta_{H_3})(1 + k \theta_{H_4})}$$

$$\text{from } \textcircled{5} \quad C_{\rho 5} = \frac{C_{\rho i}}{(1 + k \theta_{H_1})(1 + k \theta_{H_2})(1 + k \theta_{H_3})(1 + k \theta_{H_4})(1 + k \theta_{H_5})}$$

• aside to step 2

$$\textcircled{1} \quad 0 = Qc_{p_1} - Qc_{p_1} - kC_{p_1}\theta_1 \rightarrow C_{p_1} = \frac{c_{p_i}}{(1+k\theta_{H_1})}$$

$$\textcircled{2} \quad 0 = Qc_{p_1} - Qc_{p_2} - kC_{p_2}\theta_2 \rightarrow C_{p_2} = \frac{c_{p_1}}{(1+k\theta_{H_2})}$$

• sub in  $C_{p_1}$

$$C_{p_2} = \frac{c_{p_i}}{(1+k\theta_{H_1})(1+k\theta_{H_2})}$$

• similarly, develop  $C_{p_3}$  to  $C_{p_5}$

• note, if reactors are of equal volume

$$\text{then } \theta_{H_1} = \theta_{H_2}$$

$$\text{giving } C_{p_2} = \frac{c_{p_i}}{(1+k\theta_n)^2}$$

$$\text{thus, for CFSTR-}n \quad C_n = \frac{c_0}{(1+k\theta_n)^n}$$

step 3 • substitute values and solve

• calculate  $\theta_{H_i}$ :

$$\theta_{H_1} = \frac{V_1}{Q} = \frac{(8.64 \times 10^5)}{(5)} = 172800 \text{ s} \rightarrow 2 \text{ day}$$

$$\theta_{H_2} = 518400 \text{ s} \rightarrow 6 \text{ d}$$

$$\theta_{H_3} = 345600 \text{ s} \rightarrow 4 \text{ d}$$

$$\theta_{H_4} = 172800 \text{ s} \rightarrow 2 \text{ d}$$

$$\theta_{H_5} = 518400 \text{ s} \rightarrow 6 \text{ d}$$

\* note,  $\theta_H$  and  $k$  require consistent units.

$$C_{\rho_1} = \frac{(30)}{(1 + (0.2)(2))} = 21.4 \text{ g/m}^3$$

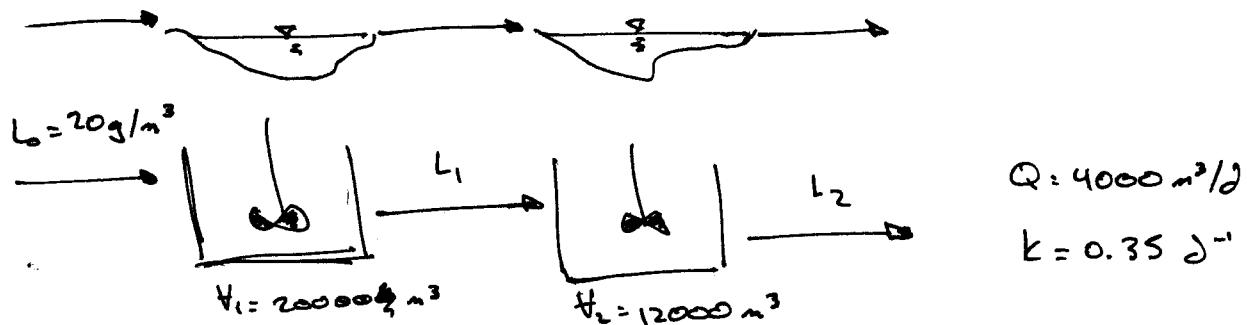
$$C_{\rho_2} = \frac{(30)}{(1 + (0.2)(2))(1 + (0.2)(6))} = 9.7 \text{ g/m}^3$$

$$C_{\rho_3} = 5.41 \text{ g/m}^3$$

$$C_{\rho_4} = 3.87 \text{ g/m}^3$$

$$C_{\rho_5} = 1.76 \text{ g/m}^3$$

- Example, ass. 3, q. 11



- solution

- assume steady-state

$$L_1 = \frac{L_0}{(1 + k \theta_{H_1})}, \quad \theta_{H_1} = \frac{H_1}{Q} = \frac{(20000)}{(4000)} = 5 \text{ d}$$

$$L_1 = \frac{(20)}{(1 + (0.35)(5))}$$

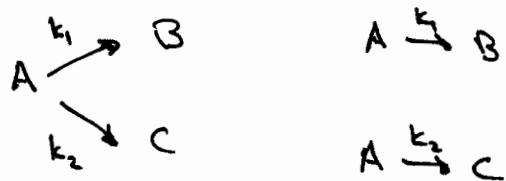
$$L_1 = 7.27 \text{ g/m}^3$$

$$L_2 = \frac{L_1}{(1 + k \theta_{H_2})}, \quad \theta_{H_2} = \frac{H_2}{Q} = \frac{(12000)}{(4000)} = 3 \text{ d}$$

$$L_2 = \frac{(7.27)}{(1 + (0.35)(3))}$$

$$L_2 = 3.55 \text{ g/m}^3$$

• example, ass3, q10 - rxn rates



• solution

• for a single first order rxn

$$\frac{dA}{dt} = -kA$$

A

• dangerous situation, parallel first order rxns

$$\frac{dA}{dt} = -k_1 A - k_2 A \quad , \text{ neg. rxn rate b/c A is being consumed}$$

$$\frac{dA}{dt} = -(k_1 + k_2) A$$

integrate:  $A = A_0 e^{-(k_1 + k_2)t}$

aside, integration to determine A expression

$$\frac{dA}{dt} = -(k_1 + k_2) A$$

$$\int \frac{1}{A} dA = -(k_1 + k_2) \int dt$$

$$\ln A + C_1 = -(k_1 + k_2) t + C_2$$

$$\ln A = -(k_1 + k_2) t + (C_2 - C_1)$$

$$A = e^{-(k_1+k_2)t} \cdot e^{(c_2-c_1)}, \quad A_0 = e^{(c_2-c_1)} = \text{const.}$$

$$A(t) = A_0 e^{-(k_1+k_2)t}$$

determine  $A_0$ , @  $t=0 \Rightarrow [A]=1 \text{ mol/L}$

$$(1) = A_0 e^{-(k_1+k_2)(0)}$$

$$A_0 = 1$$

$$\therefore A(t) = e^{-(k_1+k_2)t}$$

- sub in values & solve for  $k_1 + k_2$

@  $t=16 \text{ min} \rightarrow [A] = 0.01 \text{ mol/L}$

$$(0.01) = e^{-(k_1+k_2)(16)}$$

$$\ln(0.01) = -(k_1+k_2)(16)$$

$$k_1+k_2 = 0.287 \text{ min}^{-1}$$

B

- single first order rxn

$$\frac{dB}{dt} = k_1 A, \quad \text{pos. rxn rate b/c B is being produced}$$

$$\frac{dB}{dt} = k_1 A e^{-(k_1+k_2)t}$$

integrate:

$$B = \frac{-k_1}{k_1+k_2} A_0 e^{-(k_1+k_2)t} + D$$

+ D  
└ const. of integration

determine D, @ t=0  $\rightarrow [B] = 0 \text{ mol/L}$

$$(0) = \frac{-k_1}{k_1+k_2} A_0 e^{-(k_1+k_2)t} + D$$

$$D = \frac{k_1 A_0}{k_1+k_2}$$

$$\therefore B(t) = -\frac{k_1}{k_1+k_2} A_0 e^{-(k_1+k_2)t} + \frac{k_1 A_0}{k_1+k_2}$$

$$B(t) = -\frac{k_1}{k_1+k_2} A + \frac{k_1 A_0}{k_1+k_2}$$

$$B(t) = \frac{k_1}{k_1+k_2} (A_0 - A)$$

• sub in values to solve for  $k_1$  &  $k_2$

@ t = 16 min  $\rightarrow [A] = 0.01 \text{ mol/L}$ ,  $[B] = 0.66 \text{ mol/L}$

$$(0.66) = \frac{k_1}{k_1+k_2} ((1) - (0.01))$$

$$\frac{k_1}{k_1+k_2} = 0.667$$

from A, we know  $k_1 + k_2 = 0.287$

$$\therefore \frac{k_1}{(0.287)} = 0.667 \rightarrow k_1 = 0.191 \text{ min}^{-1}$$

$$k_2 = 0.287 - (0.191) \rightarrow k_2 = 0.096 \text{ min}^{-1}$$

C single first order rxn

$$\frac{dC}{dt} = k_2 A \quad , \text{ pos. rxn rate b/c } C \text{ is being produced}$$

$$\frac{dC}{dt} = k_2 A_0 e^{-(k_1+k_2)t}$$

$$\text{integrate: } C = -\frac{k_2}{k_1+k_2} A_0 e^{-(k_1+k_2)t} + E$$

determine  $E$ , assume @  $t=0 \rightarrow [C] = \text{not } 1/L$   
i.e. b/f rxn has started there  
is no  $C$  product.

$$(0) = -\frac{k_2}{k_1+k_2} A_0 e^{-(k_1+k_2)(0)} + E$$

$$E = \frac{k_2}{k_1+k_2} A_0$$

$$\therefore C(t) = \frac{-k_2}{k_1+k_2} A_0 e^{-(k_1+k_2)t} + \frac{k_2}{k_1+k_2} A_0$$

$$C(t) = \frac{-k_2}{k_1+k_2} A + \frac{k_2}{k_1+k_2} A_0$$

$$C(t) = \frac{k_2}{k_1+k_2} (A - A_0)$$

10 at 10

- use  $c(t)$  to populate table

<u>t (min)</u>	<u>[A] mol/L</u>	<u>[B] mol/L</u>	<u>[C] mol/L</u>
0	1.00	0	0
2	0.55	0.30	0.15
4	0.30	0.47	0.23
8	0.09	0.61	0.30
16	0.01	0.66	0.33

$$\text{e.g. } C(2) = \frac{(0.096)}{(0.287)} ((1) - (0.55))$$

$$C(2) = 0.15 \text{ mol/L}$$